## features

- Offset Voltage: $150 \mu \mathrm{~V}$ Max
- Input Bias Current: 900pA Max
- Offset Voltage Drift: $1.2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Max
- Rail-to-Rail Output Swing
- Operates with Single or Split Supplies
- Open-Loop Voltage Gain: 1 Million Min
- 1.2mA Supply Current
- Slew Rate: $0.4 \mathrm{~V} / \mu \mathrm{s}$
- Gain Bandwidth: 1.1 MHz
- Low Noise: $13 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ at 1 kHz
- Low Profile (1mm) ThinSOT ${ }^{\text {TM }}$ Package


## APPLICATIONS

- Thermocouple Amplifiers
- Bridge Transducer Conditioners
- Instrumentation Amplifiers
- Battery-Powered Systems
- Photocurrent Amplifiers

SOT-23, Rail-to-Rail Output, Picoamp Input Current Precision Op Amp DESCRIPTIOn

The LT ${ }^{\circledR 1880 ~ o p ~ a m p ~ b r i n g s ~ h i g h ~ a c c u r a c y ~ i n p u t ~ p e r f o r-~}$ mance and rail-to-rail output swing to the SOT-23 package. Input offset voltage is trimmed to less than $150 \mu \mathrm{~V}$ and the low drift maintains this accuracy over the operating temperature range. Input bias current is an ultralow 900 pA maximum.

The amplifier works on any total power supply voltage between 2.7 V and 36 V (fully specified from 5 V to $\pm 15 \mathrm{~V}$ ). Output voltage swings to within 55 mV of the negative supply and 250 mV of the positive supply, which makes the amplifier a good choice for low voltage single supply operation.

Slew rates of $0.4 \mathrm{~V} / \mu \mathrm{S}$ with a supply current of 1.2 mA give superior response and settling time performance in a low power precision amplifier.
The LT1880 is available in a 5-lead SOT-23 package.
$\boldsymbol{\mathcal { G }}$, LT, LTC, LTM, Linear Technology and the Linear logo are registered trademarks of Linear Technology Corporation. ThinSOT is a trademark of Linear Technology Corporation. All other trademarks are the property of their respective owners.

## TYPICAL APPLICATION

Precision Photodiode Amplifier

$320 \mu \mathrm{~V}$ OUTPUT OFFSET, WORST CASE OVER $0^{\circ} \mathrm{C}$ TO $70^{\circ} \mathrm{C}$ 60kHz BANDWIDTH
$5.8 \mu \mathrm{~s}$ RISE TIME, $10 \%$ TO $90 \%, 100 \mathrm{mV}$ OUTPUT STEP $52 \mu \mathrm{~V}_{\text {RMS }}$ OUTPUT NOISE, MEASURED ON A 100 kHz BW $\mathrm{V}_{\mathrm{S}}= \pm 1.5 \mathrm{~V}$ TO $\pm 18 \mathrm{~V}$
S1: SIEMENS INFINEON BPW21 PHOTODIODE ( $\sim 580 \mathrm{pF}$ )

Distribution of Input Offset Voltage

ABSOLUTE MAXIMUM RATINGS
(Note 1)
Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) ..... 40V
Differential Input Voltage (Note 2) ..... $\pm 10 \mathrm{~V}$
Input Voltage ..... $\mathrm{V}^{+}$to $\mathrm{V}^{-}$
Input Current (Note 2) ..... $\pm 10 \mathrm{~mA}$
Output Short-Circuit Duration (Note 3)
Indefinite
Operating Temperature Range (Note 4) ... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Specified Temperature Range (Note 5) .... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Maximum Junction Temperature ..... $150^{\circ} \mathrm{C}$
Storage Temperature Range

$\qquad$
$-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 10 sec ) ..... $300^{\circ} \mathrm{C}$PIn CONFIGURATIOn

## ORDER INFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING | PACKAGE DESCRIPTION | SPECIFIED TEMPERATURE RANGE |
| :--- | :--- | :--- | :--- | :--- |
| LT1880CS5\#PBF | LT1880CS5\#TRPBF | LTUM | 5-Lead Plastic TSOT-23 | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| LT1880IS5\#PBF | LT1880IS5\#TRPBF | LTVW | 5-Lead Plastic TSOT-23 | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges.
Consult LTC Marketing for information on non-standard lead based finish parts.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

ELECTRICAL CHARACTERISTICS
The $\bullet$ denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} . \mathrm{V}_{\mathrm{S}}=5 \mathrm{~V}, 0 \mathrm{~V} ; \mathrm{V}_{\mathrm{CM}}=2.5 \mathrm{~V}$ unless otherwise noted. (Note 5)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OS }}$ | Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 40 | $\begin{aligned} & 150 \\ & 200 \\ & 250 \end{aligned}$ | $\mu \mathrm{V}$ $\mu \mathrm{V}$ $\mu \mathrm{V}$ |
|  | Input Offset Voltage Drift (Note 6) | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ |  |  | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 1.2 \\ & 1.2 \end{aligned}$ | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ <br> $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| 10 S | Input Offset Current | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{A}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 150 | $\begin{gathered} 900 \\ 1200 \\ 1400 \end{gathered}$ | pA pA pA |
| $I_{B}$ | Input Bias Current | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{A}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 150 | $\begin{gathered} 900 \\ 1200 \\ 1500 \end{gathered}$ | pA pA pA |
|  | Input Noise Voltage | 0.1 Hz to 10Hz |  |  | 0.5 |  | $\mu \mathrm{Vp}$-p |
| $\mathrm{e}_{\mathrm{n}}$ | Input Noise Voltage Density | $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 13 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| $\mathrm{i}_{\mathrm{n}}$ | Input Noise Current Density | $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 0.07 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| $\mathrm{R}_{\text {IN }}$ | Input Resistance | Differential <br> Common Mode, $\mathrm{V}_{\mathrm{CM}}=1 \mathrm{~V}$ to 3.8 V |  |  | $\begin{aligned} & 380 \\ & 210 \end{aligned}$ |  | $M \Omega$ $\mathrm{G} \Omega$ |
| $\mathrm{C}_{\text {IN }}$ | Input Capacitance |  |  |  | 3.7 |  | pF |
| $\mathrm{V}_{\text {CM }}$ | Input Voltage Range |  | $\bullet$ | $\left(V^{-}+1.0\right)$ |  | $\left(\mathrm{V}^{+}-1.2\right)$ | V |

ELECTRICAL CHARACTERISTICS The • denotes the speciifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} . \mathrm{V}_{\mathrm{S}}=5 \mathrm{~V}, \mathrm{OV} ; \mathrm{V}_{\mathrm{CM}}=2.5 \mathrm{~V}$ unless otherwise noted. (Note 5)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CMRR | Common Mode Rejection Ratio | $1 \mathrm{~V}<\mathrm{V}_{\text {CM }}<3.8 \mathrm{~V}$ | $\bullet$ | 116 | 135 |  | dB |
| PSRR | Power Supply Rejection Ratio | $\mathrm{V}^{-}=0 \mathrm{~V}, \mathrm{~V}_{\text {CM }}=1.5 \mathrm{~V} ; 2.7 \mathrm{~V}<\mathrm{V}^{+}<32 \mathrm{~V}$ | $\bullet$ | 110 | 135 |  | dB |
|  | Minimum Operating Supply Voltage |  | $\bullet$ |  | 2.4 | 2.7 | V |
| AVOL | Large Signal Voltage Gain | $\begin{aligned} & R_{L}=10 k ; 1 V<V_{\text {OUT }}<4 V \\ & R_{L}=2 k ; 1 V<V_{\text {OUT }}<4 V \\ & R_{L}=1 k ; 1 V<V_{\text {OUT }}<4 V \end{aligned}$ | - | $\begin{aligned} & \hline 500 \\ & 400 \\ & 400 \\ & 300 \\ & 300 \\ & 250 \end{aligned}$ | $\begin{aligned} & 1600 \\ & 800 \\ & 400 \end{aligned}$ |  | $\mathrm{V} / \mathrm{mV}$ <br> $\mathrm{V} / \mathrm{mV}$ <br> $\mathrm{V} / \mathrm{mV}$ <br> $\mathrm{V} / \mathrm{mV}$ <br> $\mathrm{V} / \mathrm{mV}$ <br> V/mV |
| $\mathrm{V}_{\text {OL }}$ | Output Voltage Swing Low | $\begin{aligned} & \text { No Load } \\ & I_{\text {SINK }}=100 \mu \mathrm{~A} \\ & I_{\text {SINK }}=1 \mathrm{~mA} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ |  | $\begin{gathered} 20 \\ 35 \\ 130 \end{gathered}$ | $\begin{gathered} 55 \\ 65 \\ 200 \end{gathered}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ $\mathrm{mV}$ |
| $\mathrm{V}_{\mathrm{OH}}$ | Output Voltage Swing High (Referred to $\mathrm{V}^{+}$) | $\begin{aligned} & \mathrm{V}^{+}=5 \mathrm{~V} \text {; No Load } \\ & \mathrm{V}^{+}=5 \mathrm{~V} \text {; } I_{\text {SOURCE }}=100 \mu \mathrm{~A} \\ & \mathrm{~V}^{+}=5 \mathrm{~V} \text {; } I_{\text {SOURCE }}=1 \mathrm{~mA} \\ & \hline \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ |  | $\begin{aligned} & 130 \\ & 150 \\ & 220 \end{aligned}$ | $\begin{aligned} & 250 \\ & 270 \\ & 380 \end{aligned}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
| Is | Supply Current per Amplifier | $\mathrm{V}^{+}=3 \mathrm{~V}$ | $\bullet$ |  | 1.2 | $\begin{aligned} & \hline 1.8 \\ & 2.2 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
|  |  | $\mathrm{V}^{+}=5 \mathrm{~V}$ | $\bullet$ |  | 1.2 | $\begin{aligned} & 1.9 \\ & 2.3 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
|  |  | $\mathrm{V}^{+}=12 \mathrm{~V}$ | $\bullet$ |  | 1.35 | $\begin{gathered} 2 \\ 2.4 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| ISC | Short-Circuit Current | $V_{\text {OUT }}$ Short to GND $V_{\text {OUT }}$ Short to $\mathrm{V}^{+}$ | $\bullet$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 18 \\ & 20 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| GBW | Gain-Bandwidth Product | $\mathrm{f}=20 \mathrm{kHz}$ |  | 0.8 | 1.1 |  | MHz |
| $\mathrm{t}_{\text {S }}$ | Settling Time | $\begin{aligned} & 0.01 \%, V_{\text {OUT }}=1.5 \mathrm{~V} \text { to } 3.5 \mathrm{~V} \\ & A_{V}=-1, R_{L}=2 k \end{aligned}$ |  |  | 10 |  | HS |
| FPBW | Full Power Bandwidth (Note 7) | $\mathrm{V}_{\text {OUT }}=4 \mathrm{~V}_{\text {P-P }}$ |  |  | 32 |  | kHz |
| THD | Total Harmonic Distortion and Noise | $\begin{aligned} & V_{0}=2 V_{P-P}, A_{V}=-1, f=1 \mathrm{kHz}, R_{f}=1 \mathrm{k}, B W=22 \mathrm{kHz} \\ & V_{0}=2 V_{P-P}, A_{V}=1, f=1 \mathrm{kHz}, R_{L}=10 \mathrm{k}, B W=22 \mathrm{kHz} \end{aligned}$ |  |  | $\begin{gathered} 0.002 \\ 0.0008 \end{gathered}$ |  | \% |
| $\mathrm{SR}^{+}$ | Slew Rate Positive | $A_{V}=-1$ | $\bullet$ | $\begin{gathered} 0.25 \\ 0.2 \end{gathered}$ | 0.4 |  | V/ $\mu \mathrm{s}$ <br> V/ $\mu \mathrm{s}$ |
| $\overline{S R^{-}}$ | Slew Rate Negative | $A_{V}=-1$ | $\bullet$ | $\begin{aligned} & 0.25 \\ & 0.25 \\ & \hline \end{aligned}$ | 0.55 |  | $\mathrm{V} / \mu \mathrm{s}$ <br> V/ $\mu \mathrm{s}$ |

The $\bullet$ denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
$V_{S}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}$ unless otherwise noted. (Note 5)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OS }}$ | Input Offset Voltage | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 40 | $\begin{aligned} & 150 \\ & 200 \\ & 250 \end{aligned}$ | $\mu \mathrm{V}$ $\mu \mathrm{V}$ $\mu \mathrm{V}$ |
|  | Input Offset Voltage Drift (Note 6) | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 1.2 \\ & 1.2 \end{aligned}$ | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ <br> $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| los | Input Offset Current | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 150 | $\begin{gathered} \hline 900 \\ 1200 \\ 1400 \\ \hline \end{gathered}$ | pA pA pA |
| $I_{B}$ | Input Bias Current | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | $\bullet$ |  | 150 | $\begin{gathered} 900 \\ 1200 \\ 1500 \end{gathered}$ | pA $p A$ pA |
|  | Input Noise Voltage | 0.1 Hz to 10 Hz |  |  | 0.5 |  | $\mu \mathrm{V} / \mathrm{p}-\mathrm{p}$ |

ELECTRICAL CHARACTERISTICS The odentes ste speafirations wich haply were the will opeating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} . \mathrm{V}_{S}= \pm 15 \mathrm{~V}$; $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$ unless otherwise noted. (Note 5)


Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: The inputs are protected by back-to-back diodes. If the differential input voltage exceeds 10V, see Application Information, the input current should be limited to less than 10 mA .
Note 3: A heat sink may be required to keep the junction temperature below absolute maximum ratings.

Note 4: The LT1880C and LT1880I are guaranteed functional over the operating temperature range of $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.
Note 5: The LT1880C is guaranteed to meet specified performance from $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ and is designed, characterized and expected to meet specified performance from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ but is not tested or QA sampled at these temperatures. The LT18801 is guaranteed to meet specified performance from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.
Note 6: This parameter is not $100 \%$ tested.
Note 7: Full power bandwidth is calculated from the slew rate.

$$
\mathrm{FPBW}=\mathrm{SR} /\left(2 \pi \mathrm{~V}_{\mathrm{P}}\right)
$$

## TYPICAL PERFORMANCE CHARACTERISTICS



## TYPICAL PERFORMANCE CHARACTERISTICS



1880 G09b


1880 G12

Settling Time vs Output Step



1880 G10


1880 G13
Slew Rate, Gain-Bandwidth
Product and Phase Margin vs Temperature


1880 G16


## TYPICAL PERFORMANCE CHARACTERISTICS

Gain vs Frequency
with $C_{\text {LOAD }}, A_{V}=-1$


Total Harmonic Distortion + Noise vs Frequency


1880 G17B


Gain vs Frequency
with $\mathrm{C}_{\text {LOAD }}, \mathrm{A}_{\mathrm{V}}=1$


Small Signal Response

nobeo

Large Signal Response


Output Impedance vs Frequency


Small Signal Response


Large Signal Response


## APPLICATIONS InFORMATION

The LT1880 single op amp features exceptional input precision with rail-to-rail output swing. Slew rate and small signal bandwidth are superior to other amplifiers with comparable input precision. These characteristics make the LT1880 a convenient choice for precision low voltage systems and for improved AC performance in highervoltage precision systems. Obtaining beneficial advantage of the precision inherent in the amplifier depends upon proper applications circuit design and board layout.

## Preserving Input Precision

Preserving the input voltage accuracy of the LT1880 requires that the applications circuit and PC board layout do not introduce errors comparable to or greater than the $40 \mu \mathrm{~V}$ offset. Temperature differentials across the input connections can generate thermocouple voltages of 10's of microvolts. PC board layouts should keep connections to the amplifier's input pins close together and away from heat dissipating components. Aircurrents across the board can also generate temperature differentials.

The extremely low input bias currents, 150pA, allow high accuracy to be maintained with high impedance sources and feedback networks. The LT1880's low input bias currents are obtained by using a cancellation circuit on-chip. This causes the resulting $\mathrm{I}_{\text {BIAS }}{ }^{+}$and $\mathrm{I}_{\text {BIAS }}{ }^{-}$to be uncorrelated, as implied by the los specification being comparable to $I_{\text {BIAS }}$. The user should not try to balance the input resistances in each input lead, as is commonly recommended with most amplifiers. The impedance at either input should be kept as small as possible to minimize total circuit error.

PC board layout is important to insure that leakage currents do not corrupt the low $\mathrm{I}_{\text {BIAS }}$ of the amplifier. In high precision, high impedance circuits, the input pins should be surrounded by a guard ring of PC board interconnect, with the guard driven to the same common mode voltage as the amplifier inputs.

## Input Common Mode Range

The LT1880 output is able to swing nearly to each power supply rail, but the input stage is limited to operating between $\mathrm{V}^{-}+1 \mathrm{~V}$ and $\mathrm{V}^{+}-1.2 \mathrm{~V}$. Exceeding this common mode range will cause the gain to drop to zero, however no gain reversal will occur.

## Input Protection

The inverting and noninverting input pins of the LT1880 have limited on-chip protection. ESD protection is provided to prevent damage during handling. The input transistors have voltage clamping and limiting resistors to protect against input differentials up to 10 V . Short transients above this level will also be tolerated. If the input pins can see a sustained differential voltage above 10 V , external limiting resistors should be used to prevent damage to the amplifier. A 1 k resistor in each input lead will provide protection against a 30 V differential voltage.

## Capacitive Loads

The LT1880 can drive capacitive loads up to 600pF in unity gain. The capacitive load driving capability increases as the amplifier is used in higher gain configurations, see the graph labled Capacitive Load Response. Capacitive Ioad driving may be increased by decoupling the capacitance from the output with a small resistance.

## Capacitance Load Response



1880 G25

## Getting Rail-to-Rail Operation without Rail-to-Rail Inputs

The LT1880 does not have rail-to-rail inputs, but for most inverting applications and noninverting gain applications, this is largely inconsequential. Figure 1 shows the basic op amp configurations, what happens to the op amp inputs, and whether or not the op amp must have rail-to-rail inputs.

APPLICATIONS INFORMATION


INVERTING: $A_{V}=-R_{F} / R_{G}$ OP AMP INPUTS DO NOT MOVE, BUT ARE FIXED AT DC BIAS POINT V $V_{\text {REF }}$

INPUT DOES NOT HAVE TO BE RAIL-TO-RAIL


NONINVERTING: $A_{V}=1+R_{F} / R_{G}$ INPUTS MOVE BY AS MUCH AS $V_{\text {IN }}$, BUT THE OUTPUT MOVES MORE

INPUT MAY NOT HAVE TO BE RAIL-TO-RAIL


NONINVERTING: $A_{V}=+1$ INPUTS MOVE AS MUCH AS OUTPUT

INPUT MUST BE
RAIL-TO-RAIL FOR OVERALL CIRCUIT RAIL-TO-RAIL PERFORMANCE

Figure 1. Some Op Amp Configurations Do Not Require Rail-to Rail Inputs to Achieve Rail-to-Rail Outputs

The circuit of Figure 2 shows an extreme example of the inverting case. The input voltage at the 1M resistor can swing $\pm 13.5 \mathrm{~V}$ and the LT1880 will output an inverted, divided-by-ten version of the input voltage. The input accuracy is limited by the resistors to $0.2 \%$. Output referred, this error becomes 2.7 mV . The $40 \mu \mathrm{~V}$ input offset voltage contribution, plus the additional error due to input bias current times the $\sim 100 \mathrm{k}$ effective source impedance, contribute only negligibly to error.


Figure 2. Extreme Inverting Case: Circuit Operates Properly with Input Voltage Swing Well Outside Op Amp Supply Rails.

## Precision Photodiode Amplifier

Photodiode amplifiers usually employ JFET op amps because of their low bias current; however, when precision is required, JFET op amps are generally inadequate due to their relatively high input offset voltage and drift. The LT1880 provides a high degree of precision with very low bias current ( $l_{B}=150 \mathrm{pA}$ typical) and is therefore applicable to this demanding task. Figure 3 shows an LT1880 configured as a transimpedance photodiode amplifier.


Figure 3. Precision Photodiode Amplifier

## APPLICATIONS InFORMATION

The transimpedance gain is set to $51.1 \mathrm{k} \Omega$ by $\mathrm{R}_{\mathrm{F}}$. The feedback capacitor, $\mathrm{C}_{\mathrm{F}}$, may be as large as desired where response time is not an issue, or it may be selected for maximally flat response and highest possible bandwidth given a photodiode capacitance $C_{D}$. Figure 4 shows a chart of $C_{F}$ and rise time versus $C_{D}$ for maximally flat response. Total output offset is below $262 \mu \mathrm{~V}$, worst-case, over temperature $\left(0^{\circ} \mathrm{C}\right.$ to $\left.70^{\circ} \mathrm{C}\right)$. With a 5 V output swing, this guarantees a minimum 86dB dynamic range over temperature $\left(0^{\circ} \mathrm{C}\right.$ to $\left.70^{\circ} \mathrm{C}\right)$, and a full-scale photodiode current of $98 \mu \mathrm{~A}$.

## Single-Supply Current Source for Platinum RTD

The precision, Iow bias current input stage of the LT1880 makes it ideal for precision integrators and current sources. Figure 5 shows the LT1880 providing a simple precision current source for a remote $1 \mathrm{k} \Omega$ RTD on a 4 -wire


Figure 4. Feedback $C_{F}$ and Rise Time vs Photodiode $C_{D}$
connection. The LT1634 reference places 1.25 V at the noninverting input of the LT1880, which then maintains its inverting input at the same voltage by driving 1 mA of current through the RTD and the total $1.25 \mathrm{k} \Omega$ of resistance set by R1 and R2. Imprecise components R4 and C1 ensure circuit stability, which would otherwise be excessively dependant on the cable characteristics. R5 is also noncritical and is included to improve ESD immunity and decouple any cable capacitance from the LT1880's output. The 4-wire cable allows Kelvin sensing of the RTD voltage while excluding the cable IR drops fromthe voltage reading. With 1 mA excitation, a $1 \mathrm{k} \Omega$ RTD will have 1 V across it at $0^{\circ} \mathrm{C}$, and $+3.85 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ temperature response. This voltage can be easily read in myriad ways, with the best method depending on the temperature region to be emphasized and the particular ADC that will be reading the voltage.


Figure 5. Single Supply Current Source for Platinum RTD

## SImPLIFIGD SCHEmATIC



## PACKAGE DESCRIPTION

S5 Package
5-Lead Plastic TSOT-23
(Reference LTC DWG \# 05-08-1635)


1. DIMENSIONS ARE IN MILLIMETERS
2. DRAWING NOT TO SCALE
. DIMEN
ARE EXCLUSIVE OF MOLD FLASHANDMEAL BURR
3. MOLD FLASH SHALL NOT EXCEED 0.254 mm
4. JEDEC PACKAGE REFERENCE IS MO-193

## TYPICAL APPLICATION

All SOT-23 JFET Input Transimpedance Photodiode Amplifier


## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :--- | :--- | :--- |
| LT1782 | Rugged, General Purpose SOT-23 Op Amp | Rail-to-Rail I/O |
| LT1792 | Low Noise JFET Op Amp | $4.2 n \mathrm{~V} / \sqrt{\mathrm{Hz}}$ |
| LT1881/LT1882 | Dual/Quad Precision Op Amps | $50 \mu \mathrm{~V} \mathrm{~V}_{\text {OS(MAX) , 200pA }}$ I $\mathrm{B}(\mathrm{MAX})$ Rail-to-Rail Output |
| LTC2050 | Zero Drift Op Amp in SOT-23 | $3 \mu \mathrm{~V} \mathrm{~V}_{\text {OS(MAX), Rail-to-Rail Output }}$ |
| LT6010 | 135 $\mu \mathrm{A}$ Rail-to-Rail Output Precision Op Amp | Lower Power Version of LT1880 |

